



# Amorphous-silicon thin-film transistors deposited by VHF-PECVD and hot-wire CVD

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## Abstract

We investigate the impact of new growth techniques on the mobility and stability of amorphous silicon (a-Si:H) thin film transistors (TFTs). It was suggested that the key parameter controlling the field-effect mobility and stability is the intrinsic mechanical stress in the a-Si:H layer. We study a series of bottom-gate TFTs incorporating a-Si:H deposited by VHF PECVD and hot-wire CVD. All TFTs exhibit good characteristics with mobilities of 0.6–0.7 cm<sup>2</sup>/V s. The mean activation energy  $E_A$  and the slope of the barrier-height distribution  $k_B T_0$  for defect creation in the a-Si:H are determined.  $E_A$  correlates to the intrinsic stress. © 2002 Elsevier Science B.V. All rights reserved.

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## 1. Introduction

Amorphous silicon (a-Si:H) thin film transistors (TFT), commonly deposited by plasma enhance chemical vapor deposition (PECVD) at 13.56 MHz, are widely used as pixel-switching devices in large-area electronics. The low field-effect mobility (< 1 cm<sup>2</sup>/V s) and the limited stability under gate-bias stress, due to defect creation in the a-Si:H, complicates the utilization in applications where high performance is demanded, such as OLED displays and column/row-addressing circuitry. While the low mobility is attributed to the inherent disorder of a-Si:H, the microscopic details of the

defect-creation mechanism (Staebler–Wronski effect) are still elusive.

TFTs incorporating PECVD a-Si:H with high compressive stress exhibited a poor stability [1]. This was explained with a high fraction of short (compressed) Si–Si bonds, of which the energy levels are located in the valence-band tail, which tend to break under charge accumulation, thereby forming dangling-bond defects. This process is thermally activated with an exponential distribution of barrier heights.

Since ‘device-quality’ a-Si:H usually has high compressive stress, combining a high field-effect mobility with a high TFT stability seems to be contradictory. Therefore, alternative deposition techniques, such as very-high frequency (VHF) PECVD [2] and hot-wire (HW) CVD [3] have been used for TFT deposition. It could be shown that

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TFTs with a high stability, maintaining a high mobility, are feasible [4]. We now present a comprehensive study of the stability and mobility of VHF and hot-wire TFTs.

## 2. Amorphous silicon deposition and material properties

The a-Si:H layers and TFTs for this study were deposited in the ultrahigh vacuum multi-chamber deposition system ASTER (electrode area 177 cm<sup>2</sup>). Plasma excitation frequencies of 13.56, 30, 50, and 70 MHz were used. The substrate temperature was 250 °C; we used hydrogen-diluted silane (SiH<sub>4</sub>/H<sub>2</sub> = 30 sccm/30 sccm). In order to remain in the  $\alpha$ -regime with a deposition rate around 0.2 nm/s we reduced the pressure and the plasma power with increasing frequency.

Additionally, a-Si:H was deposited by HWCVD. Two tantalum filaments heated to 1900 °C and mounted 5 cm underneath parallel to the substrate were utilized to catalytically decompose pure silane. The substrate temperature was 340 °C. The deposition rate was 1.34 nm/s.

From the Si–H stretching mode at 2000 cm<sup>-1</sup> of infrared absorption spectra (FTIR) we determined a hydrogen concentration of 11–12 at.% for the plasma a-Si:H, slightly decreasing with increasing frequency. The hot-wire a-Si:H had a hydrogen content of 8.3 at.%. We attributed the lower value to the higher substrate temperature. A shoulder at

2090 cm<sup>-1</sup> in the FTIR spectrum is generally attributed to Si–H<sub>2</sub> or Si–H vibrations on internal surfaces. The spectra of the plasma a-Si:H show very little microstructure, while for the hot-wire material a microstructure parameter of  $R^* = I_{2090}/(I_{2000} + I_{2090}) = 0.2$  indicates Si–H<sub>2</sub> and/or microvoids.

The mechanical stress in 150–320 nm thick a-Si:H films on ultra flat thin glass substrates (Schott D263) was calculated by the beam-bending method from the parabolic curvature of the substrate [5], measured with a Dektak profilometer and cross-checked with a laser-scanning method [1]. To obtain the intrinsic stress  $\sigma_i$  in the a-Si:H we subtracted the stress component due to the mismatch of the thermal expansion coefficient of the substrate and the film,  $\sigma_{th} = E_f/(1 - \nu_f) \cdot (a_s - a_f) \cdot (T_s - T_{room})$ . We used  $a_s = 7.2 \times 10^{-6} \text{ K}^{-1}$ ,  $a_f = 4 \times 10^{-6} \text{ K}^{-1}$ , and  $\nu_f = 0.2$  [1]. The Young's modulus was taken as  $E_f = 140 \text{ GPa}$  for all a-Si:H films. This is expected for PECVD a-Si:H with 12 at.% hydrogen [1]. Literature values for HWCVD a-Si:H with around 8 at.% hydrogen vary between 110 and 140 GPa ([6] and references therein). For our samples  $\sigma_{th}$  was 130 and 180 MPa for  $T_s = 250$  and 340 °C, respectively. The resulting intrinsic (compressive) stress  $\sigma_i$  ranges between 90 and 540 MPa. We estimate a relative error of  $\pm 50 \text{ MPa}$ , mainly due to the thickness inhomogeneity of the a-Si:H films. An overview over the deposition parameters and material properties is given in Table 1.

Table 1  
Deposition parameters and properties of PECVD and HWCVD a-Si:H layers and TFTs

	PECVD				HW
<i>a-Si:H</i>					
<i>f</i> (MHz)	13.56	30	50	70	–
<i>p</i> (Pa)	40	30	20	10	2
<i>P</i> (mW/cm <sup>2</sup> )	57	40	28	11	–
Thickness (nm)	244	151	219	320	268
<i>r</i> <sub>dep</sub> (nm/s)	0.20	0.13	0.17	0.27	1.34
[H] (at.%)	11.9	11.7	11.4	10.7	8.3
$\sigma_i$ (MPa)	540	255	450	360	85
<i>TFT</i>					
$\mu_{FE}$ (cm <sup>2</sup> /V s)	0.64	0.68	0.72	0.70	0.61
$k_B T_0$ (meV)	63	64	65	65	63
$E_A$ (eV)	0.918	0.929	0.916	0.922	0.937

### 3. Thin film transistors

The a-Si:H layers were incorporated in bottom-gate TFTs with a nitrogen-rich PECVD a-SiN<sub>x</sub> gate dielectric as described elsewhere [7]. The device structure was: glass substrate/Cr gate contact/300 nm a-SiN<sub>x</sub>/200 nm a-Si:H/50 nm n<sup>+</sup> a-Si:H/Cr–Al source-drain contacts. Different layers were deposited in dedicated chambers of the multi-chamber system. Inverted-staggered TFTs were made by conventional back-channel etching. The channel dimensions were  $W/L = 11\,520\ \mu\text{m}/50\ \mu\text{m}$ .

Fig. 1 shows the linear transfer characteristics of some TFTs. All devices exhibit good characteristics, with a low off current, a steep sub-threshold swing of  $S \sim 0.3\ \text{V}/\text{dec}$ , and without charge trapping. The initial threshold voltages were  $V_t^{\text{ini}} = (2 \pm 0.2)\ \text{V}$  with very little spread between different devices. The field-effect mobilities reach  $0.72\ \text{cm}^2/\text{V s}$  exhibiting a slight increase with increasing plasma frequency. Values determined in saturation regime ( $V_g = V_{\text{sd}}$ ) did not differ substantially. Table 1 summarizes the TFT properties.

For determining the TFT stability, we applied a gate voltage of  $V_g = 25\ \text{V}$  at temperatures between 312 and 370 K for up to 28 h. To determine the threshold voltage  $V_t$ , the bias stress was briefly interrupted to measure the linear transfer charac-

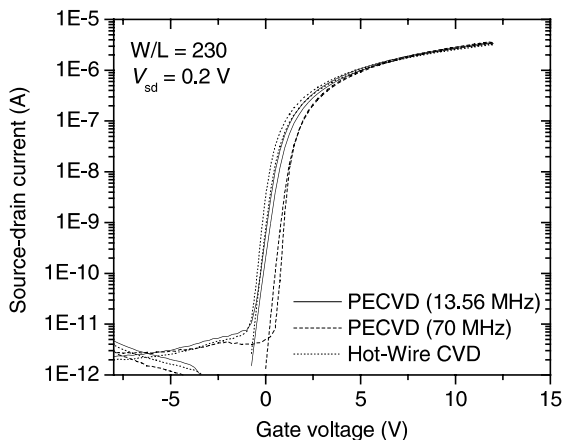


Fig. 1. Linear transfer characteristics (sweeping in both directions) of VHF-PECVD and HWCVD a-Si:H TFTs.

teristics at the stressing temperature. Fig. 2 shows the result of the 13.56 MHz sample. The data was interpreted within the framework of the thermalization-energy concept [8] by fitting a stretched hyperbola function [1,8] to the relative threshold-voltage shift

$$\begin{aligned} (V_t - V_t^{\text{ini}})/(V_g - V_t^{\text{ini}}) \\ = 1 - (\exp[(E_{\text{th}} - E_A)/k_B T_0] + 1)^{-1/(\alpha-1)}, \end{aligned}$$

with  $E_{\text{th}} = k_B T \ln(v_0 t)$  being the thermalization energy. The equation describes dispersive defect creation, thermally activated with an exponential distribution of barrier heights, and a superlinear ( $\alpha$ ) dependence on the band-tail carrier density. The best overlap of data sets from different temperatures was obtained with an ‘attempt-to-break’ frequency of  $v_0 = 10^9\ \text{s}^{-1}$ , slightly lower than the  $10^{10}\ \text{s}^{-1}$  as previously found for a-Si:H TFTs [4,8]. The best fitting results were obtained with  $\alpha = 1.5$ . A discussion on the meaning of this parameter is found elsewhere [9].

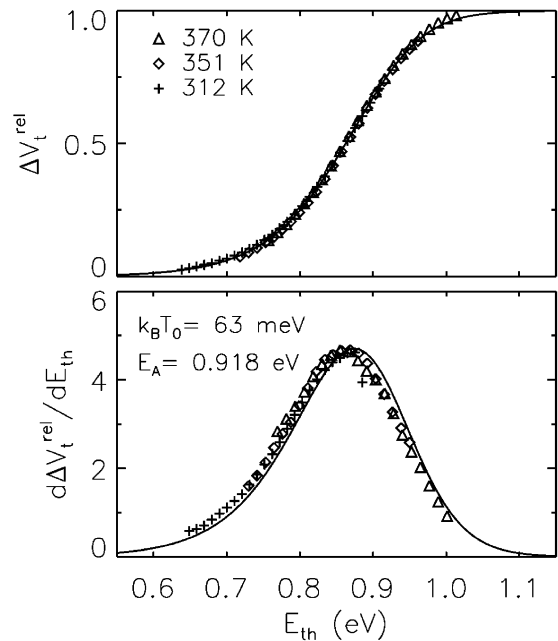


Fig. 2. Relative threshold voltage shift versus thermalization energy (top), and the derivative (bottom), for the 13.56 MHz PECVD a-Si:H TFT; experimental data ( $v_0 = 10^9\ \text{s}^{-1}$ ) and a least-squares fit with a stretched hyperbola ( $\alpha = 1.5$ ).

Physically meaningful parameters, such as the mean activation energy for defect creation,  $E_A$ , and the slope of the barrier-height distribution,  $k_B T_0$  can be extracted from the derivative of  $\Delta V_t(E_{th})$ , namely, the peak position and its width, respectively (Fig. 2). We found  $k_B T_0$  to be between 63 and 65 meV, comparable to  $k_B T_0$ s as previously reported for PECVD and HWCVD a-Si:H TFTs with these mobilities [1,4]. The activation energy  $E_A$  ranges between 0.916 and 0.937 eV  $\pm$  0.005 eV.

Fig. 3(a) shows  $E_A$  versus  $\sigma_i$ . As expected, a trend towards higher  $E_A$  for lower compressive stress is present. In order to cross-check this, we performed Raman spectroscopy (excitation wavelength 514.5 nm) on the a-Si:H films. The peak position of the transverse-optic (TO) mode  $\omega_{TO}$ , determined within an accuracy of  $\pm 0.5$   $\text{cm}^{-1}$ , was reported to shift towards higher wave numbers for higher compressive stress [10]. Fig. 3(b) shows that  $E_A$  indeed decrease with increasing  $\omega_{TO}$ , confirming the trend in Fig. 3(a).

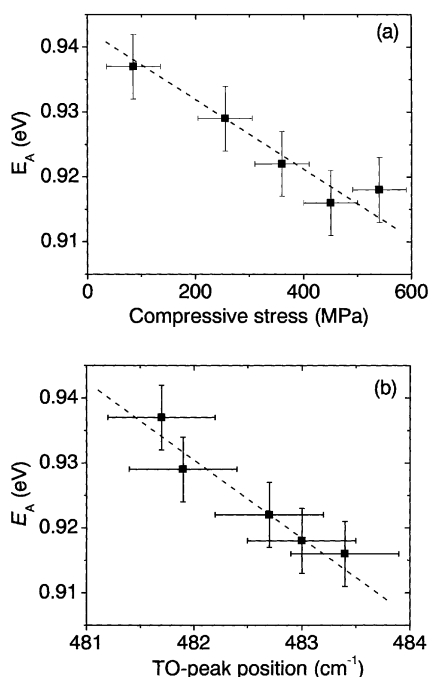


Fig. 3. Activation energy for defect creation versus (a) intrinsic stress and (b) the peak position of the TO-like band in Raman spectra.

#### 4. Discussion

At first sight, the TFTs seem to be very similar, with the same characteristics, threshold voltages and field-effect mobilities in a narrow range 0.61–0.72  $\text{cm}^2/\text{V s}$ . This is a success on its own, since it demonstrates that HWCVD a-Si:H, deposited with a much higher growth rate, can replace PECVD a-Si:H in TFTs with similar mobility and an even better stability. The slightly lower value of the mobility of the HWCVD a-Si:H TFT can be explained with the higher  $R^*$  and a higher Urbach energy of  $E_0 = 55$  meV, as derived from Constant Photocurrent Method (CPM) absorption spectra. The PECVD a-Si:H, in comparison, have  $R^* < 0.05$  and  $E_0 \sim 50$  meV. In the case of the PECVD TFTs, the slight increase of  $\mu_{FE}$  with increasing plasma frequency and decreasing power is supposed to be due to the softer plasma conditions resulting in less a-Si:H/a-SiN<sub>x</sub> interface damage, thus a lower trap density.

The dispersion parameter  $k_B T_0$  is assumed to be dependent on the degree of order of the material in the channel. Similarly, the width of the TO-like band is linked to the bond-angle distribution (near-range order) in the Si network [11]. Since also the field-effect mobility was found to be related to the material order [12], a correlation between these three parameters could be expected. However, we found no correlation, which might be due to the low spread in experimental data.

Compact ‘device-quality’ a-Si:H is generally found to be under compressive stress. Less dense a-Si:H, as deposited by PECVD in the  $\gamma'$ -regime at high deposition rates, tends to contain microvoids and has tensile stress. In plasma a-Si:H, the origin of compressive stress is commonly ascribed to the ion bombardment. At deposition temperatures  $< 300$  °C the ion energy is needed to increase the surface mobility of growth precursors and to enable the cross-linking process for obtaining a dense network. Excessive ion energy leads to ion implantation a few monolayers underneath the surface; thus, the surplus of Si atoms results in a densification and compressive stress [13]. Hence, the variation of stress in our PECVD films can be explained with a variation in ion energies due to the different deposition conditions. In the case of

HWCVD no ion bombardment is present; thus, another mechanism must be responsible for inducing compressive stress. For remote-plasma deposition the compressive stress was ascribed to the invasive incorporation of hydrogen into the rigid Si network [14]. Since the key features are similar in HWCVD (high atomic hydrogen flux, no ion bombardment), the same effect might hold.

Even though the trend in Fig. 3(a) is obvious, HWCVD a-Si:H deposited with higher  $T_s$  cannot be simply included into the diagram. We find  $\sigma_i = 170$  MPa in hot-wire a-Si:H deposited at 430 °C. TFTs with this a-Si:H reach  $E_A > 1$  eV [4]. Plotting it in Fig 3(a) would lead to a sharp peak around 200 MPa, which was indeed found in [1] for PECVD TFTs. However, while the intrinsic stress may be the parameter primarily determining  $E_A$  for PECVD a-Si:H, we doubt that the intrinsic stress is in general the *only* parameter determining  $E_A$ , as becomes clear by considering high- $T$  HWCVD a-Si:H.

It was shown [15] that ‘device-quality’ HWCVD a-Si:H with a low hydrogen content is highly inhomogeneous containing microvoids and hydrogen clusters, hence, the origin of a macroscopic parameter, such as the intrinsic stress, is complex and might be misleading. To explain the superior stability of HWCVD a-Si:H deposited at high  $T_s$ , the inhomogeneous structure and/or hydrogen distribution might play a direct role. The intrinsic stress may be an indirect parameter or be dominant for low- $T$  a-Si:H only. However, more detailed conclusion are beyond the scope of this paper and require a more thorough study.

## 5. Conclusions

We demonstrated that state-of-the-art TFTs with mobilities of 0.6–0.7 cm<sup>2</sup>/V s can be made by using VHF-PECVD and HWCVD a-Si:H. In particular, high deposition rate hot-wire a-Si:H leads to TFTs with comparable characteristics and even superior stability.

We found an increasing TFT stability with decreasing compressive stress in the a-Si:H. Al-

though for HWCVD a-Si:H the concept of intrinsic stress being the key parameter controlling the stability seems problematic, our results confirm the previously reported data of PECVD a-Si:H TFTs.

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